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PIPSI/NAVY-RAPID EVALUATION OF PROPULSION SYSTEM EFFECTS FOR THE NAVY GAS TURBINE ENGINE CODE, NEPCOMP

W. H. Ball
The Boeing Company
Seattle, Washington 98124



11 October 1979

Final Report for Period 28 June 1979 through 11 October 1979

Contract No. N62269-79-C-0278

Approved for Public Release; Distribution Unlimited

Prepared for NAVAL AIR DEVELOPMENT CENTER Warminster, Pennsylvania 18974

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This report describes the work accomplished of to modify two existing interactive computer pengine performance, including inlet and nozzl their use for NADC.	during a fourteen-week contract programs for calculating installed be corrections and to demonstrate
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FOREWORD

This report describes the work performed at The Boeing Company on Contract N62269-79-C-0278. The work was performed during the period 28 June through 3 October 1979.

During the contract the existing PIPSI and DERIVP computer codes previously developed for the U.S. Air Force were modified to operate on the NADC computer system and a training session was held at NADC to explain the operation of the codes and to demonstrate its usage to NADC personnel.

Mr. John Cyrus was Project Monitor for NADC and Mr. W. H. Ball was Program Manager for The Boeing Company. Modifications to the computer code were accomplished by Mr. R. A. Atkins, Jr.

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LIST OF NOMENCLATURE AND SYMBOLS

A _C	Inlet capture area, in2
Ao	Local stream tube area ahead of the inlet, in2
AoI	Free-stream tube area of air entering the inlet, in2
c_D	Drag coefficient, $\frac{D}{q A_{ref}}$, dimensionless
C-D	Convergent-divergent
$c_{D_{ADD}}$	Additive drag coefficient, $C_{D_{ADD}} = \frac{D_{ADD}}{q A_c}$, dimensionless
$c_{D_{A10}}$	Afterbody drag coefficient, DRAG, dimensionless
CDBase	Base drag coefficient, $(P_b - P_{\infty}) A_{base}$, dimensionless
^C D _{A10-A9} ,	. 10
$c_{D_{PAP}}$	Drag coefficient, $q_0(A_{10}-A_9)$, based on projected area, dimensionless
C _{fG} , Cv	Thrust coefficient, $\frac{F_g}{\psi_{Q(x)}}$, dimensionless
D	Thrust coefficient, $\frac{F_g}{\frac{\dot{w}}{g}(V_1)}$, dimensionless Drag, lb.; hydraulic Diameter, $\frac{4A}{P}$, in., diameter, in.
F _N	Net thrust, 1b.
$F_{N_{A}}$	Installed net thrust, lb.
М	Mach number, dimensionless
P _T	Total pressure, 1b/in2
PT ₂ /PT ₀	Total pressure recovery
SFC	Specific fuel consumption
SFCA	Installed specific fuel consumption
T/F	Turbofan
T/J	Turbojet
W	Mass flow, lb/sec
$W_{C}, \frac{w\sqrt{\delta}}{\delta}$	Corrected airflow, 1b/sec.
0 ₇₂	Temperature correction factor, TT ₂ /1STD.
N	2-D nozzle wedge half-angle
Р	Round plug nozzle half-angle

INTRODUCTION

The purpose of the contract work was to modify an existing Air Force/
Boeing computer code (PIPSI, documented in References 1 through 4),
install the modified code on the NADC CDC computer system, and train NADC
personnel in the usage of the code by means of instruction and
demonstration.

The complete documentation of the calculation methods employed by the code, nomenclature, sample cases, and the library of inlet and nozzle/aftbody input maps is contained in the set of documents (References 1 through 4) which describe the code developed for the Air Force version of the program. This report describes those changes to the existing code that were made to adapt the code to the NADC computer and to provide the desired output data.

MODIFICATIONS TO PIPSI CODE

The modifications to the computer code that were accomplished to make the code compatible with the NADC computer system and the NADC input data format are described below.

Changes in Uninstalled Engine Data Format

(1) The format of the uninstalled engine data for the NADC version of the PIPSI program is slightly different from that described in Section 6.6 of Reference 2. The engine input data format for the NADC PIPSI code is shown in Figure 1. The only difference from the original code is that the areas input for A8 and A9, shown in

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Figure 1 NADC Uninstalled Engine Data Input Format (Continued)

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Figure 1 NADC Uninstalled Engine Data Input Format (Continued)

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Figure 1 NADC Uninstalled Engine Data Input Format (Concluded)

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columns 8 and 9 respectively, are input in square inches for the NADC input instead of in square feet as in the Air Force version of the PIPSI code. The square inches are converted internally (in the revised code) to square feet.

(2) The association of external file names to internal program tape definitions is done with GET statements rather than ATTACH statements. For instance,

use GET, TAPE1=AFE to connect TAPE1 with previously stored AFE (Uninstalled engine input data file).

also, GET, TAPES1 = inlet file

GET,TAPE5? = aftbody file

GET, TAPE53 = CFG file

GET, TAPE54 = capture area file

(3) The code was modified to automatically generate installed propulsion system performance output data for use in mission performance calculations. This data is written to an output file named TAPE7. This file is automatically generated with each execution of the PIPSI program. The format for the TAPE7 output is as shown in Figure 2. The format was provided by NADC at the start of the contract work.

The modifications, debugging, checkout, sample calculations, and demonstration were all performed using the NADC computer system. At the

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Figure 2 Format for TAPE7 (Installed Performarie) File(Continued)

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Figure 2 Format for TAPE7 (Installed Performance) File (Conciuded)

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beginning of the contract, a magnetic tape containing the existing Air Force versions of the source codes for the PIPSI and DERIVP plus a complete library file of inlet performance, nozzle/aftbody drag maps, and nozzle $^{\rm CF}_{\rm G}$ maps was mailed to NADC and was installed by NADC personnel as permanent files in their CDC computer system. The modifications were then accomplished by Boeing personnel using a remote access keyboard terminal located at Seattle, Washington.

Preparation of ADEN Nozzle Maps

A set of nozzle/aftbody drag and $C_{\mbox{F}_{\mbox{G}}}$ maps for the ADEN CD Nozzle was developed for use during the installed performance calculations. These maps for the ADEN configuration are described and shown in Appendix A.

Calculation of Installed Performance

After the source code was modified, binary (object) deck files were created and stored as permanent files in the NADC computer. After the modified object decks were obtained, a series of installed performance calculations was performed using the matrix of engines, inlets, nozzle/aftbody drag maps, and nozzle $C_{\mbox{\scriptsize F}_{\mbox{\scriptsize G}}}$ maps described in Appendix A. Plotted results from some of the installed performance calculations are contained in Appendix A. Appendix A also contains a catalog of the files stored in the NADC computer with key files indicated.

Demonstration and Training Session

At the conclusion of the contract work, a training session was held at NADC to explain and demonstrate the operation of the computer programs to

NADC personnel. Appendix B contains some of the general briefing charts that were contained in handout material distributed to the NADC personnel who participated in the training sessions. The charts are presented in Appendix B to provide a source of information for those who want to learn of the general operating characteristics of the computer programs without obtaining the complete set of documents describing the programs (References 1 through 4).

APPENDIX A

INSTALLED PERFORMANCE CALCULATIONS

TABLE A-I

SUMMARY OF INSTALLED PERFORMANCE CALCULATIONS

UNINSTALLED ENGINE DATA	INLET	NLET DATA	AFTBODY DRAG DATA	JDY JATA	NOZ CF	NOZZLE C _{F,} DATA	DETAILED INSTALLED PERFORMANCE OUTPUT	"MARK II" MISSION PERFORMANCE DECK
FILE NAME	CONFIG.	NAME	CONFIG.	NAME	CONFIG.	NAME	FILE NAME	FILE NAME
BOEING1	2	F8	6	ADENCD	S	CVADEN	FSTFD	F8TFDM
(DRY THRBAFAN)	<u>ب</u> ک	NS NS NS	თ თ	ADENCD ADENCD	ഗ വ	CVADEN CVADEN	NSTFD NS2TFD	NSTFDM NS2TFDM
	o ~ ∞	LWF	, o o	ADENCO	ഹഹ	CVADEN	LWFTFD ATSTFD	LWFTFDM ATSTFDM
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TURBOFAN)	တ	NS2	5	ADENCO	5	CVADEN	NS2TFW	NS2TFWM
	_	LWF	6	ADENCO	2	CVADEN	LWFTFW	LWFTFWM
	. ω	ATS2	6	ADENCD	2	CVADEN	ATSTFW	ATSFTWM
BONGTJD	2	85	თ	ADENCD	Ŋ	CVADEN	F8TJD	F8TJDM
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TURBOJET	9	NS2	ნ	ADENCD	5	CVADEN	NS21JD	NS2TJDM
	^	FX	ᢐ	ADENCD	2	CVADEN	LWFTJD	LWFTJDM
	. ∞	ATS2	6	ADENCD	2	CVADEN	ATSTJD	ATSTJDM
RONGTJW	2	85	6	ADENCD	2	CVADEN	F8TJW	F8TJWM
(A/B	ц	SN	O	ADENCO	2	CVADEN	MCTSN	MNCTSN
THRROJET)	9	NS2	ത	ADENCD	2	CVADEN	NS21JW	NS2TJWM
	^	I M.H	6	ADENCD	5	CVADEN	LWFTOW	LWFTUWM
	. σ	ATS2	6	ADENCD	5	CVADEN	ATSTJW	ATSTOWM

TABLE A-II
SUMMARY OF INLET CAPTURE AREAS

				w 75-	P _{T2}	Ao	A _c ,
INLET CONFIG.	MACH	ALT.	ENG. TYPE	$\frac{W\sqrt{\theta_2}}{\delta_2}$	PTO	$\frac{A_0}{A_c}$	FT ²
	.80	50000.	T/F	330.	.98	. 74	9.183
F8	.80	50000.	T/J	284.	.98	.74	7.903
	.60	50000.	T/F	331.	.967	.975	7.882
NS	.60	50000.	T/J	284.	.967	.977	6.763
	.80	50000.	T/F	330.	.982	.95	7.168
NS2	.80	50000.	T/J	284.	.982	.95	6.169
	.80	50000.	T/F	330.	. 965	.77	8.690
LWF	.80	50000.	T/J	284.	. 965	.77	7.479
	2.00	50000.	T/F	234.	.925	.915	8.079
ATS2	1.60	50000.	T/J	256.	.948	.872	7.042

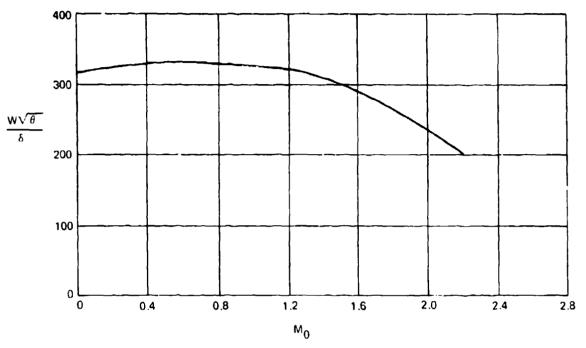


Figure A-1. Maximum Engine Airflow for Turbofan Engine

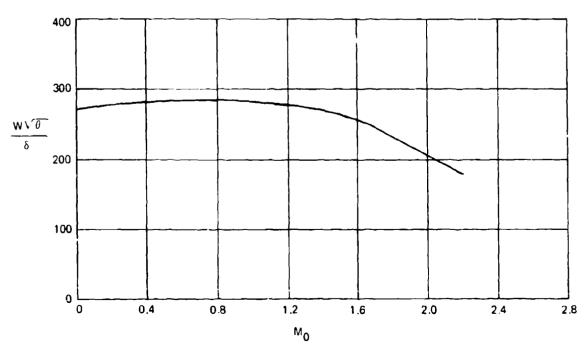


Figure A-2. Maximum Engine Airflow for Turbojet Engine

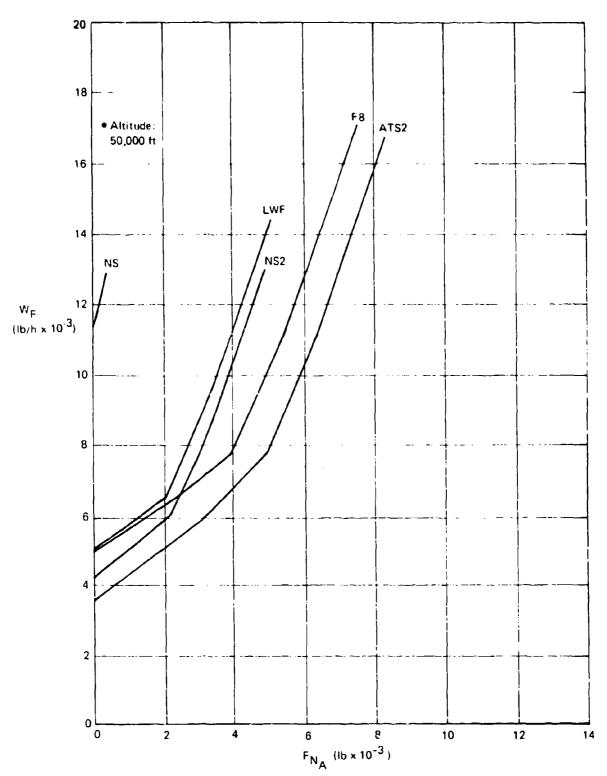


Figure A-3. Comparison of Installed Performance for Various Inlet Configurations at Mach 2.0 (Turbofan Engine)

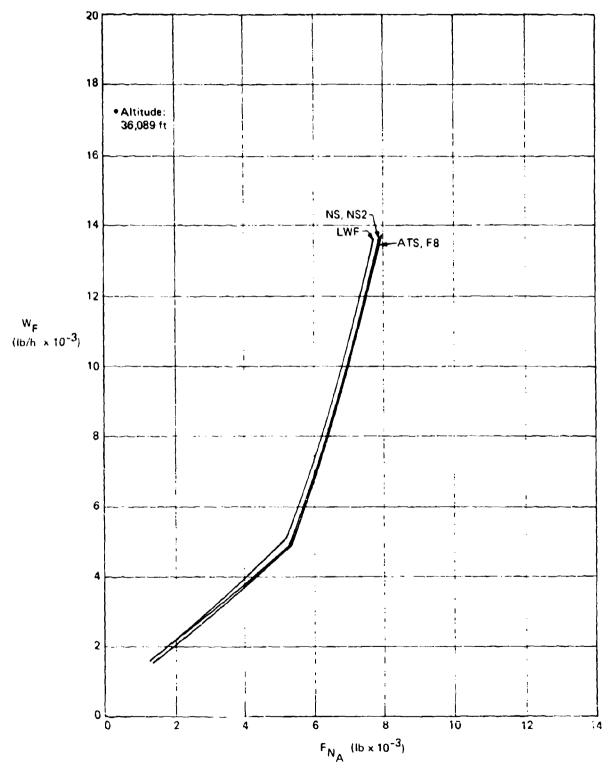


Figure A-4. Comparison of Installed Performance for Various Inlet Configurations at Mach 0.80 (Turbofan Engine)

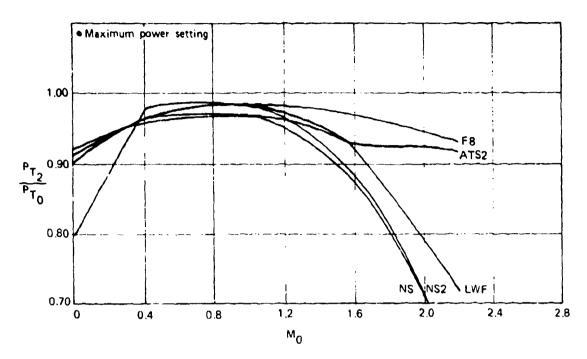


Figure A-5. Comparison of Matched Inlet Total Pressure Recovery for Various Inlets (Turbofan Engine)

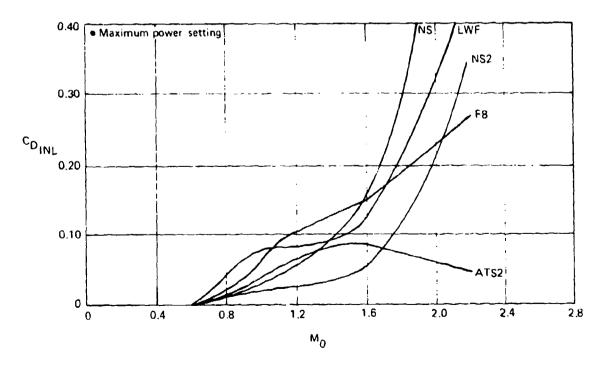


Figure A-6. Comparison of Matched Inlet Drag for Various Inlet (Turbofan Engine)

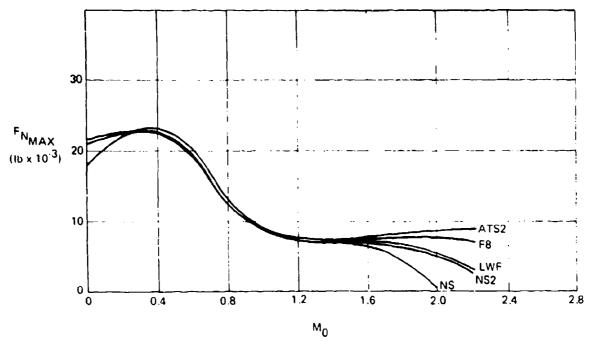


Figure A-7. Comparison of Maximum Installed Thrust for Various Inlets (Turbofan Engine)

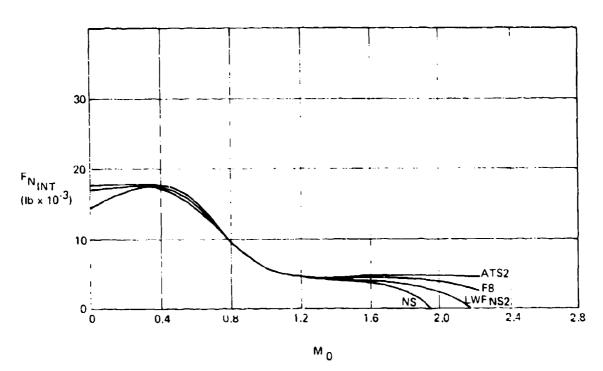


Figure A-8. Comparison of Intermediate Installed Thrust for Various Inlets (Turbofan Engine)

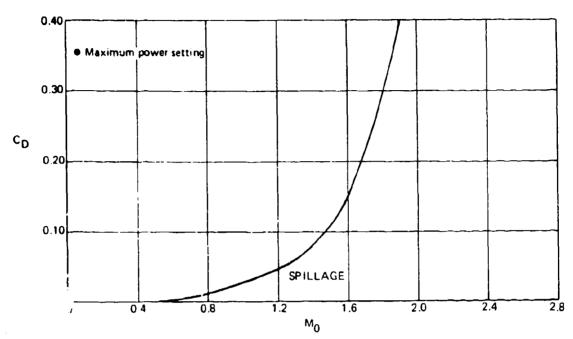


Figure A.9. Inlet Drag for a Normal Shock Inlet With a Turbofan Engine

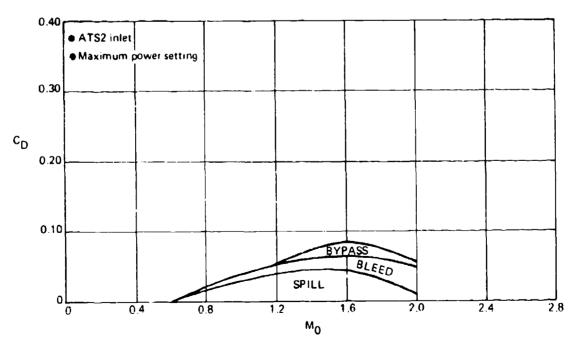


Figure A.10. Inlet Drag for a Mach 2.0 Inlet With a Turbofan Engine

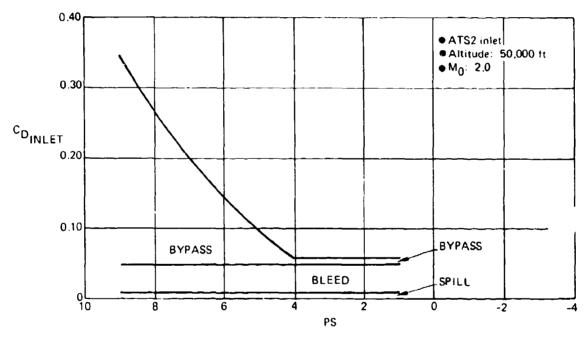


Figure A-11. Inlet Drag Versus Power Setting for a Mach 2 Inlet With a Turbofan Engine

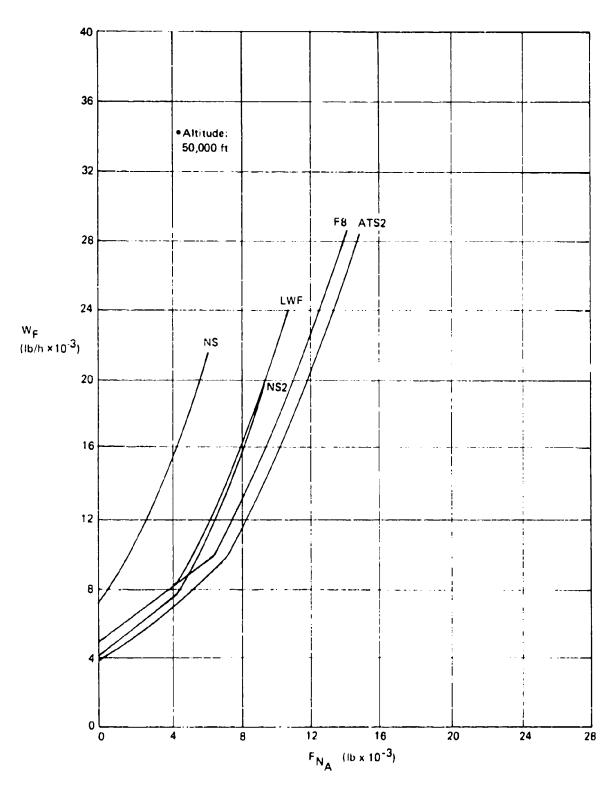


Figure A-12. Comparison of Installed Performance for Various Inlet Configurations at Mach 2.0 (Turbojet Engine)

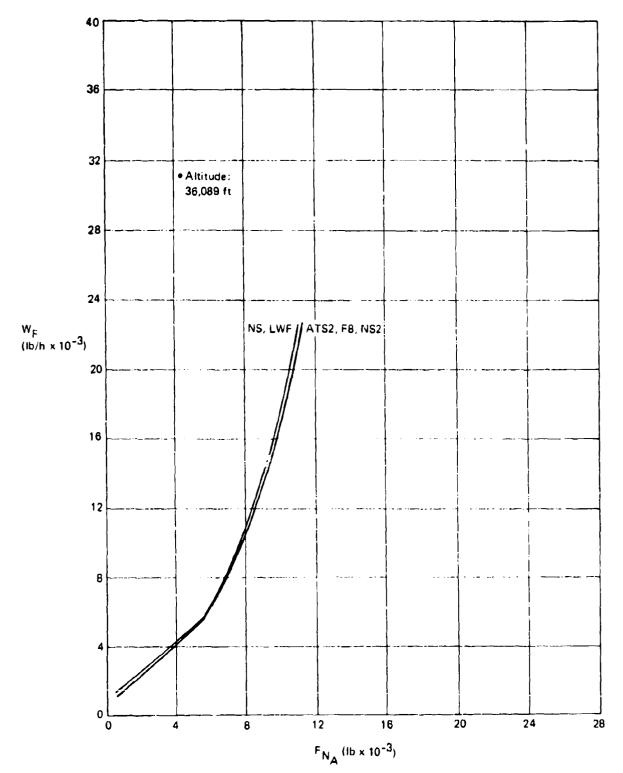


Figure A-13. Comparison of Installed Performance for Various Inlet Configurations at Mach 0.80 (Turbojet Engine)

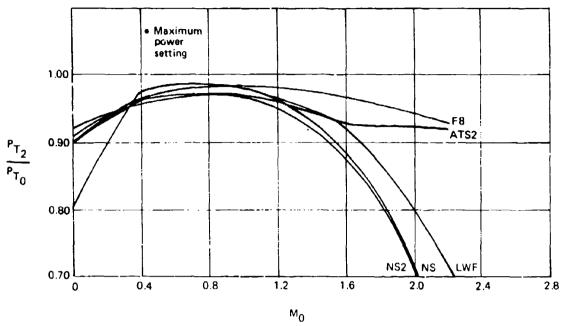


Figure A-14. Comparison of Matched Inlet Total Pressure Recovery for Various Inlets (Turbojet Engine)

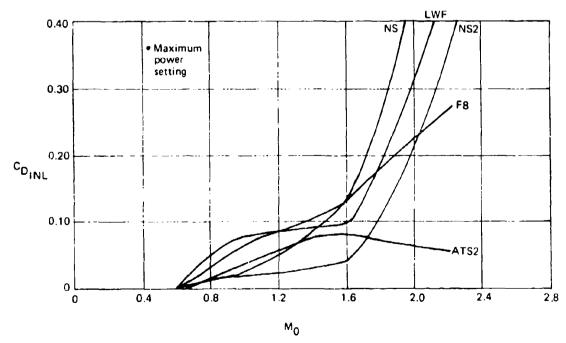


Figure A-15. Comparison of Matched Inlet Drag for Various Inlets (Turbojet Engine)

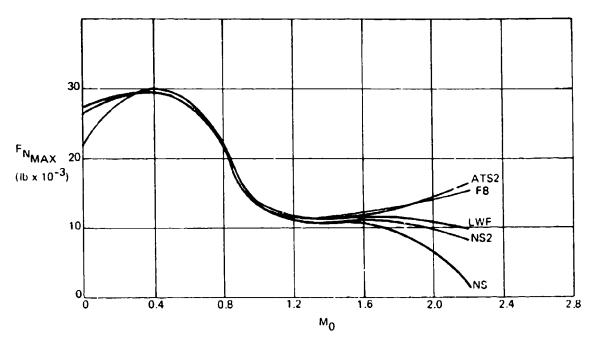


Figure A-16. Comparison of Maximum Installed Thrust for Various Inlets (Turbojet Engine)

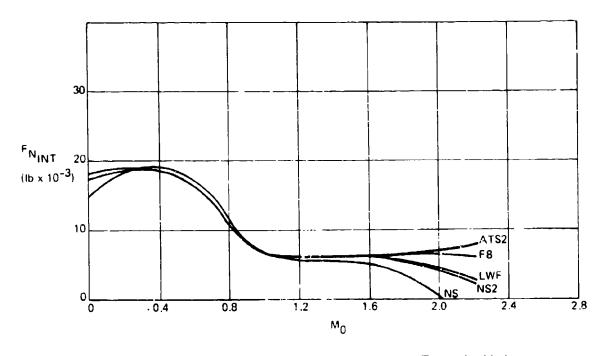


Figure A-17. Comparison of Intermediate Installed Thrust for Various Inlets (Turbojet Engine)

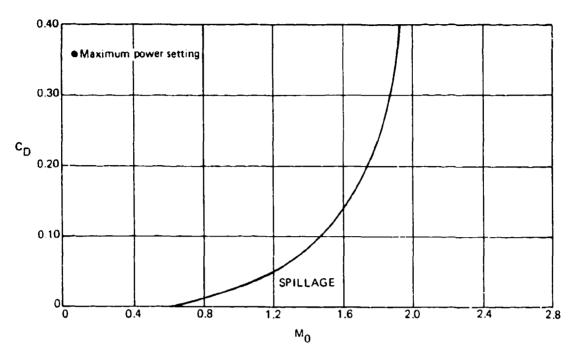


Figure A-18. Inlet Drag for a Normal Shock Inlet With a Turbojet Engine

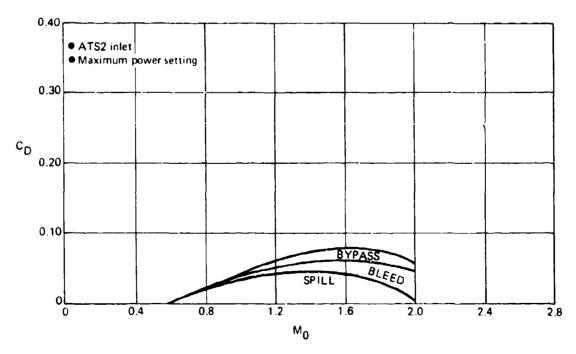


Figure A-19. Inlet Drag for a Mach 2.0 Inlet With a Turbojet Engine

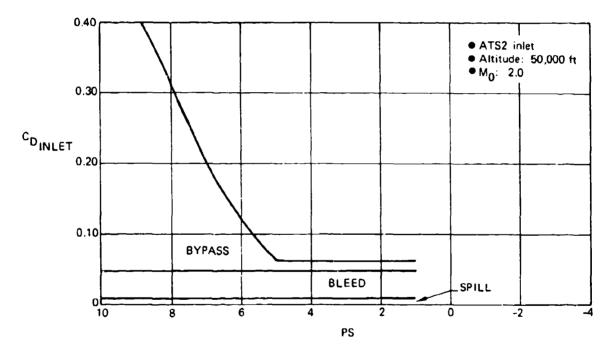


Figure A-20. Inlet Drag Versus Power Setting for a Mach 2.0 Inlet With a Turbojet Engine

CATALOG OF 603293

79/10/09. 12.54.06

FILE NAME (S)

ACIM31 ATSTJI BOEING1 CV2I	ACIM36 ATSTJIM BOEING2 CU2D1	ADENCI ATSTJW BUSTJD CV2D6	AIAA ATSTJWM BONGTJW ENGDEKM	ATSTFIM ATS2 CUADEN F8	ATSTFN ATS2IM3 CUADEN2 FSTFD	ATSTFWM BILOUT CV1 FSTFDM
FETFN	FETFUM	F8TFWM1	FETFN2	FBTFW3	FETFUSM	F8TFN4
FETFW4M	FE:TUI	FSTJIM	FEITLIN	F8TJWM	LWF	LHFTFI
LNETFIM	LNFTFW	LWFTFWM	LNFTJI	LNFTJIM	LWFTJW	LWFTJWM
MAFX1	M9SUE	NADC3	MADCSE	NADC4	NAIC4B	NADC7
NAIC7B	NADCSB	NADCAB	NS .	NSTFI	MSTFIM	MSTFW
NSTFUM	MSTUD	MSTUDM	HSTUN	MSTUMM	NSS	NS2TFD
NSETFIM	MSZTFW	MSSTFWM	NSETUD	MILTSRM	NSETUN	MSSTUNM
MUTEST	NU7	MUSIF1	NUSIFE	HUSTO	TAPE7	TESTOUT
USER	WEARIN	NPABDPE	XXXX	208NTTY		

89 FILES(S)

REALY

FILE NAME	FILE CONTENTS
BOE ING1	Dry Turbofan Engine Uninstalled Data
BOEING2	Afterburning Turbofan Engine Uninstalled Data
BONGTJD	Dry Turbojet Engine Uninstalled Data
BONGTJW	Afterburning Turbojet Engine Uninstalled Data
NADC7	Source Deck for PIPSI Program
NADC9B	Object Deck for PIPSI Program
WPABDP	Source Deck for Derivative Process Program
WPABDPB	Object Deck for Derivative Process Program
MAPXI	Library File of Inlet, Nozzle/Aftbody Drag, and Nozzle ${\sf C_F}_{\sf G}$ Maps
CVADEN	ADEN Nozzle C _{F G} Map
ADENCD	Nozzle/Aftbody Drag Map for ADEN Nczzle

Figure A-21 Catalog of Permanent Files on NADC Computer Account

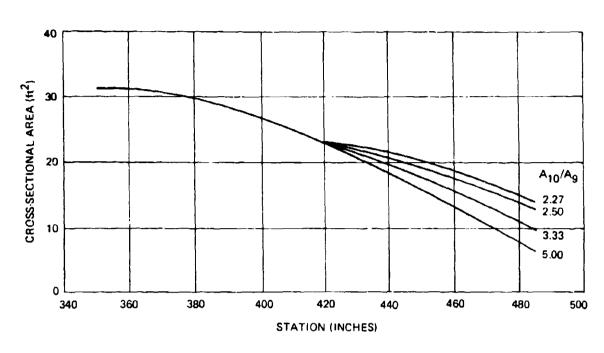


Figure A-22. Nozzle and Aftbody Area Distribution for a Twin ADEN Nozzle Configuration

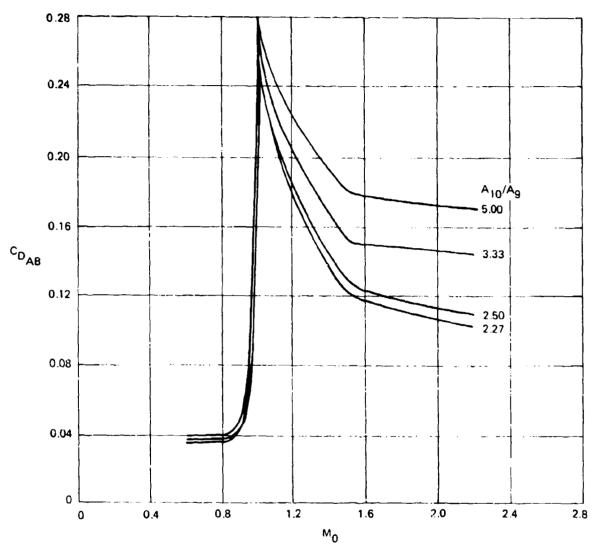


Figure A-23. Drag for a Twin ADEN Nozzle Configuration

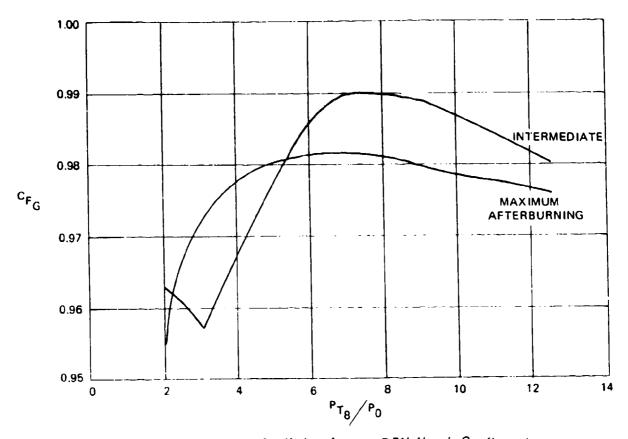


Figure A-24. Gross Thrust Coefficient for an ADEN Nozzle Configuration

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APPENDIX B

GENERAL COMPUTER PROGRAM OPERATING CHARACTERISTICS

What is PIPSI?

- An improved version of a computerized engineering procedure designed to calculate installed propulsion system performance for preliminary design studies of advanced military aircraft.
- A previous version of the program (P.I.P.S.) was supplied to the Air Force as part of contract F33615-72-C-1580.
- The engineering procedure used in the original study was designated P.I.T.A.P. (Propulsion Installation and Table Assembly Program; ref: AFFDL-TR-72-147, vols I-IV).
- P I P S I program is documented in AFFDL-TR-78-91, Vols I-IV July 1978.

Figure B-1 Description of PIPSI Program and References

Preliminary Analysis Process Using PIPSI

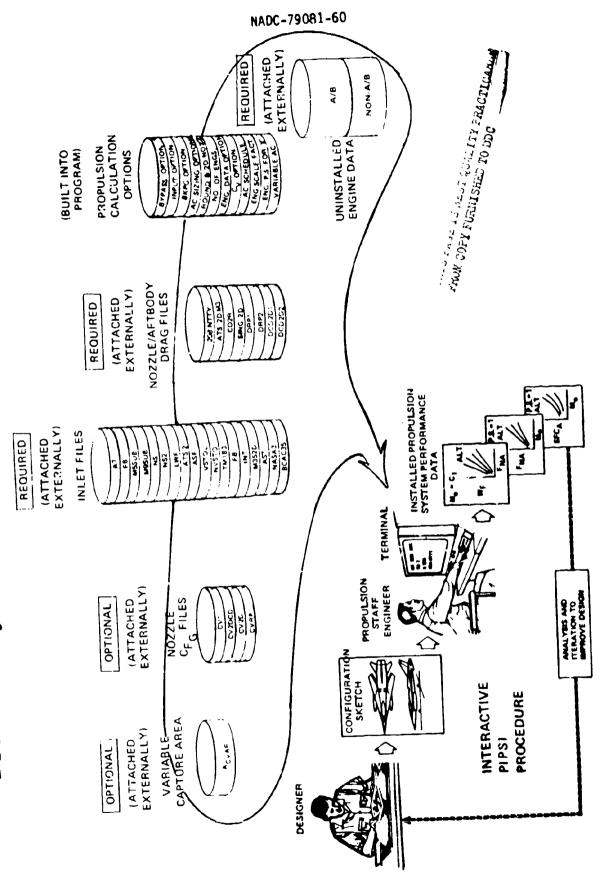


Figure B-2 PIPSI Analysis Process and Files Utilized

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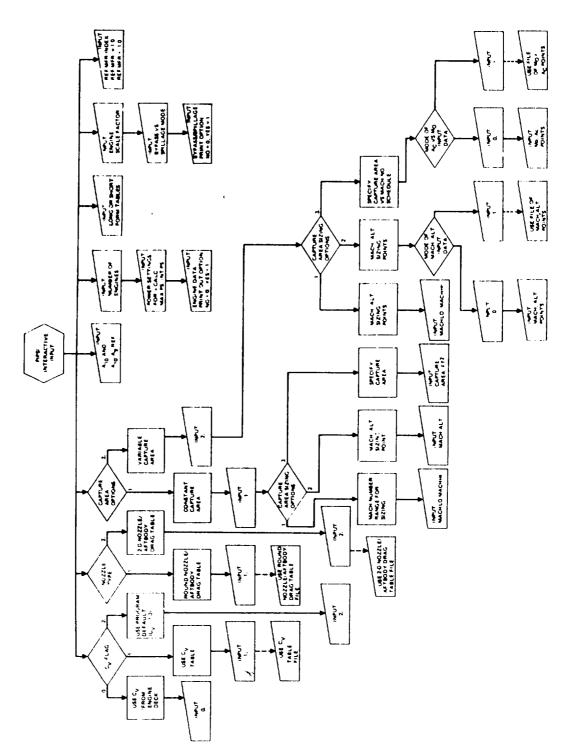


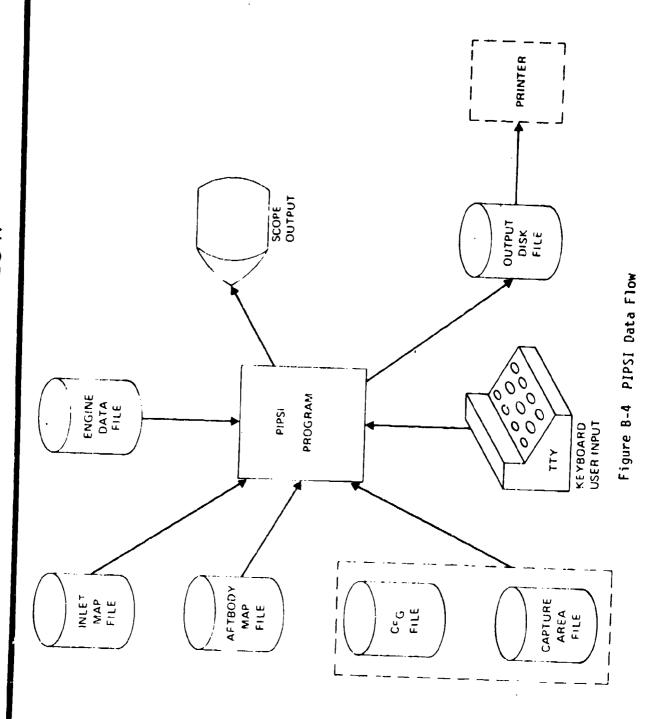
Figure B-3 PIPSI Interactive Input Options

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PIPSI Data Flow

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Matrix of Inlet Maps

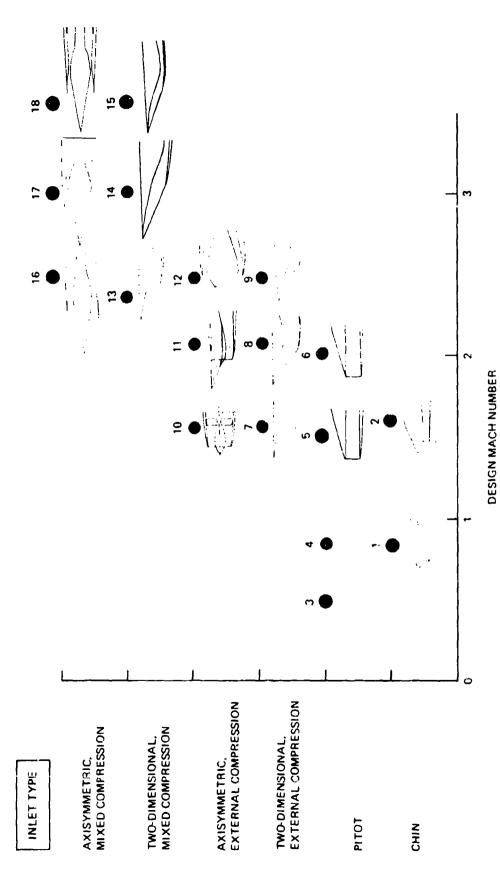


Figure B-5 Matrix of Inlet Maps in Library File

Matrix of Nozzle Types

DRAG	DC02	DCD2.	20 20	ats 20m3
3 A	CV 2D- CO	CV 2D-CV	CV2D SING.	CV2D ATS 2DM3
2-DIMENSIONAL				
	CONVERGENT-DIVERGENT		PLUG (WEDGE)	
AXISYMMETRIC		AA		AA
DRAG	208N- TT-	.CV1 CD2R	 	ORP2
S A A A A B	ર્ક	نې	CVRP DRP1	CV RP

Figure B-6 Matrix of Nozzle Maps in Library File

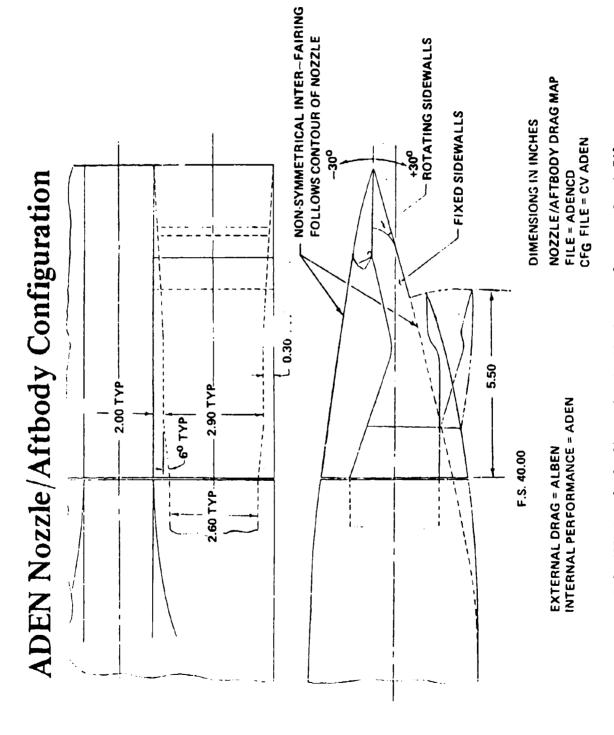


Figure B-7 ADEN Nozzle Configuration Available as a Separate Input File

The Derivative Process

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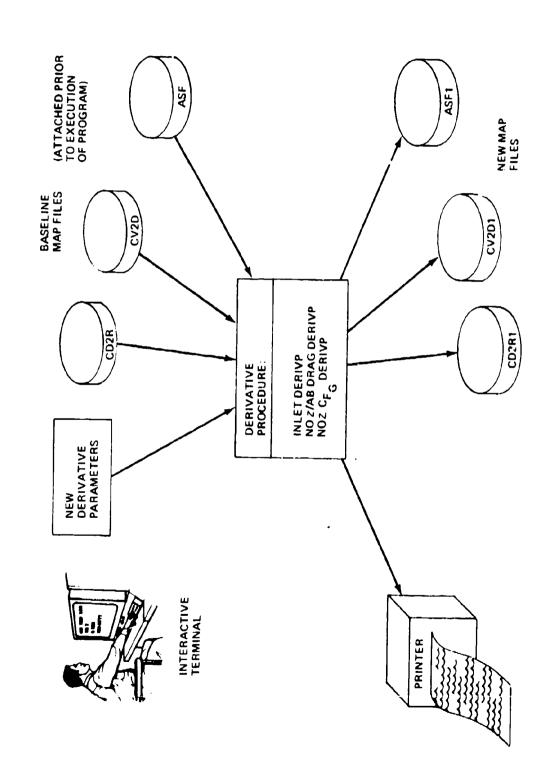


Figure 8-8 Illustration of the Derivative Process

```
한>GET • NADC78 • THFE1= BOEING1.TAPE51=ATS2 • THFE5은=ADENCD.THFE5S=CVADEN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             INPUT NUMBER OF ENGINES AND ENGINE SCALE FACTOR
                                                                                                                                                INPUT NOZZLE THPUST COEFFICIENT(CV) FLAG WHERE
                                                                                                                                                                                                                                                                                                                                                                                                                INPUT CAPTURE AREA OPTION WHERE
COONSTANT CAPTURE AREA±1.,VARIABLE OPTION=2.)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             172. .9
IMPUT POWER SETTINGS FOR GANMA CALCULATION
                                                                                                                                                                                                                    FOR CV=1.(PROGRAM DEFAULT)
                                                                                                                                                                     FOR CV FROM ENGINE DECK
                                                                                                                                                                                              FOR CV FROM CV TABLE
                                                                                                                                                                                                                                                                                                                  MOZZLE=1. FOP POUND MOZZLE
MOZZLE=2. FOR 2-D MOZZLE
                                                                                                                                                                                                                                                                                            INPUT NOZZLE TYPE WHERE
                                                                                                                                                                                                                                                                                                                                          MOZZLE=2. FOR
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                                                                                                   RFL,60000.
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                                                    HOLESAN TOR
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                                                                                                                                                                                                                       2=70
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MANAGARIA DOGO COLONIA STATINA (NAMIMUM POWER SETTING AND INTERMEDIATE POWER SETTING)

Figure B-9. Example of a PIPSI Terminal Session (Continued)

INPUT ENGINE PPINT OPTION(NO=1, VES=2.)

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INPUT REFERENCE MASS FLOW PATIO INDEX

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BARRA MARKE INDEX WHERE
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                                       EXCESS INLET AIRFLOW
                                                                             FOR MIN
                    EXCESS INLET AIRFLOW BYPASSED ABOVE MOSBP
EXCESS INLET HIRFLOW SPILLED EXTERNALLY
                                                          OPTIMUM COMBINATION OF BYPASS AND SPILLAGE OPTIMUM COMBINATION OF BYPASS AND SPILLAGE
                                        SCHEDULED BYPASS WITH REST OF
                                                                             OPTIMUM COMBINATION OF
                        그
                                                                MMDDE=4.
                                                                                   MODE=5.
                                            KMDDE=3.
      XMODE=1.
                         MMODE=2.
```

O. OTHERWISE FOR BYPASS MODE PRINT DUT ENTER 1.

0. IF THE INLET MAP FILE ENTER 1. IF ONLY RECOVERY AND DRAG MARS ARE ON THE ENTER INLET MAP FILE ALL INLET MAPS

1. MMLDJUMHI (SIZING ENVELOPE OPTION) INPUT ONE OF THE FOLLOWING CODES INCET SIZING INPUTS

3. ACAPI (INPUI CAPTURE AREA - SQ 2. MACHIALT (SIZING POINT OPTION)

INPUT XMLD AND XMHI(SIZING ENVELOPE OPTION)

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	1.00 XMOZF6=	O SCALE =	0 H10H9R=	U REFMFR =	= IHWE 0	CTION DESIRED
	1.0	○. N	(}) }- च	0.0	ا <u>ت</u> ا •	COPPE
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	150	11	H	H	11	-
0) () ()	CVFLAG=	ENGIN	ĒĪĒ. □	OF LEP	MMLO =	ENTER

9.60 9.60 9.60

Example of a PIPSI Terminal Session (Continued) Figure B-9.

INLET SIZING DATA

ALT60000. 00. POINT MACH 4.670 SQ FT INLET SIZING POINT CAPTURE AREA 4.670

BEGIN PROCESSING MARK12 DECK AIR FORCE TEST CASE

INPUT NOZZLE THRUST COEFFICIENT(CV) FLAG WHERE ÇV=0 FOR CV FROM EMBINE DECK CV FROM CV THBLE $0 = \triangle 0$ 0=\n\) [:\:-1

CV=1.(PROGRAM DEFAULT) FIDE FIDE

4.157 CP SECONDS EXECUTION TIME C > DISPOSE (TAPE6=PR/EI=VT0004) I>"END"

C > DISPOSE, TAPE7=PV

Windows October One Property of the Manager of the

Figure B-9. Example of a PIPSI Terminal Session (Concluded)

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FAPE2=CD2R TAPE53=CV1		VE PROCESSOR PROGRAM
CD2R		980
TAPE2=		ESSO
`• o		PECC
=NVST		176
TAPE51=NVSTO		DERIVATIVE
PB . 1		DER
WFABD	WPABDPB	
SET . WPABDPB T	AW V	
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MVSTD INLET

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.1200 9.0000

TOTAL WALL ANGLECDEGS

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OTED SAUS

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Figure B-10. Example of a DERIVP Terminal Session (Continued)

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INPLIT NUMBER OF PAPAMETERS TO BE CHANGED
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INPUT THE PARAMETERS ID BE CHANGED FOLLOWED BY THE NEW VALUES IN PAIRS(PARAMETER NUMBER,NEW VALUE)

ING 20, 4 2.3 18 .2 PARAMETER NUMBER 3 FIRST RAMP ANGLE(DEG) A PESTAN MACH NUMBER

NEW VALUE 20.0000 2.3000 .2000

> DESIGN MACH NUMBER SUBSONIC DIFFUSER LOSS COEFFICIENT

> > 0,

DERIVATIVE PROCESSOR PROGRAM

ARE THE DERIVATIVE PARAMETERS CORRECT(0=YES

ENTER CODE FOR NAPS TO BE CHANGED 1 FOR INLET NAP CHANGES 2 FOR NOZZLE/AFTBODY CHANGES

POR CV MAP CHANGES

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0 \

CDER INPUT MAP

ENTER CODE FOR OUTPUT DESIRED O FOR TAPEG OUTPUT ONLY 1 FOR TAPEG OUTPUT HAD DERIVATIVE PPOCESSOR FILE

1>0

AFTERBODY MAP DERIVATIVE PARAMETERS TAIL FIN FORE AND AFT LOCATION RATIO PAPAMETER DEFINITION NOZZLE STATIC PRESSURE RATIO AFTERBODY TYPE = CD-AXISYMMETRIC DUAL NOZZLE THIL FIN COMPIGURATION FIN PROLECTES) BASE APEA RATIO THIL PARAMETER NUMBER 4 10

OLD VALUE

1.0000 2.0000 0.0000 1735 0.0000

Figure B-10. Example of a DERIVP Terminal Session (Continued)

INPUT NUMBER OF PARAMETERS TO BE CHANSED

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INPUT THE PARAMETERS TO BE CHAMBED FOLLOWED BY THE NEW VALUES IN PAIRS(PARAMETER NUMBER, NEW VALUE)

PARAMETER DEFINITION FIN FORE AND AFT LOCATION PATIO BASE AREA RATIO TAIL PARAMETER NUMBER 154 .0 5 .1

NEW VALUE .2000 .1000

ARE DERIVATIVE PARAMETERS CORRECTIONSYES 1=NO)

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25.(1)

637.00 44.50 700.00 41.50 760.00 36.00 800.00 830.00 20.50 876.00 17.84

TABLE NUMBER = 3 A10.49 = 3.33 STATION AND APER

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Figure B-10. Example of a DERIVP Terminal Session (Continued)

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gog ol sen sikang vigo mag.
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Example of a DERLV? Terminal Session (Continued) Figure B-10.

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DERIVATIVE PROCESSOR PROGRAM

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2 FOR NOZZLEZAFTBODY CHANGES
3 FOR CV MAP CHANGES

When I to the little walls to the state waster

1 >3

CV1 INPUT MAP

ENTER CODE FOR OUTPUT DESIRED O FOR TAPES OUTPUT ONLY 1 FOR TAPES OUTPUT AND TAPE! (NEW PIPS!)

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NOZZLE TYPE = ROUND CONVERGENT-DIVEPGENT NOZZLE
CFG MAP DEPIVATIVE PAPAMETERS
PARAMETER DEPINITION
DIVERGENCE HALF ANGLICES)

OLD VALUE 11.4500

INPUT NUMBER OF PARAMETERS TO BE CHANGED

1>1

INPUT THE PAPAMETEPS TO BE CHANGED FOLLOWED BY THE NEW VALUE IN PAIPS(PAPAMETER WIMBER.MEW VALUE)

Figure B-10. Example of a DERIVP Termina! Session (Continued) PARAMETER DEFINITION DIVEPGENCE HALF ANGLECTES PAPAMETER NUMBER 121 12.5

NEW YALUE 12.5000

1=10) APE THE DEPIVATIVE PAPAMETERS COPRECT(0=YES

0 ^ 1

DERIVATIVE PROCESSOR PROGPAM

ENTER CODE FOR MARS TO BE CHAMGED
1 FOR INLET MAR CHAMGES
2 FOR MOZZLE/AFTBODY CHAMGES
3 FOR CV MAR CHAMGES

I >"END"

7.520 CP SECONDS EXECUTION TIME C>DISPUSE: (TAPE6=PR/EI=VT0004)

C > DISPOSE(TAPE1=PR/E1=VT0004)

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Figure B-10. Example of a DERIVP Terminal Session (Concluded)

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REFERENCES

- 1. Ball, W. H., and Hickcox, T. E., Rapid Evaluation of Propulsion System Effects, Volume 1 Final Report, AFFDL-TR-78-91, Vol. I, Air Force Flight Dynamics Laboratory, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio 45433, July 1978.
- 2. Ball, W. H., and Atkins, R. A., Jr., Rapid Evaluation of Propulsion System Effects, Volume II PIPSI Users Manual, AFFDL-TR-78-91, Vol. II, Air Force Flight Dynamics Laboratory, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio, 45433, July 1978.
- 3. Hickcox, T. E., Atkins, R. A. Jr., and Ball, W. H., Rapid Evaluation of Propulsion System Effects, Volume III Derivative Procedure (DERIVP) Users Manual, AFDL-TR-78-91, Vol. III, Air Force Flight Dynamics Laboratory, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio, 45433, July 1978.
- 4. Ball, W. H., Rapid Evaluation of Propulsion System Effects, Volume IV Library of Configurations and Performance Maps, AFFDL-TR-78-91, Volume IV, Air Force Flight Dynamics Laboratory, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio, 45433, July 1978.

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